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## Filtering performances of 20 protective fabrics against solid aerosols

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### ABSTRACT

Workers can be exposed to solid airborne particles in some occupational environments, and they might be required to wear chemical protective clothing to prevent skin exposure. Dedicated standards exist to certify the protective value of such clothing, but they are not informative enough to identify the main pathways of entry for solid particles nor to compare performances between different chemical protective clothing. In this work, 20 non-woven fabrics used to make chemical protective clothing for solid particle protection were selected to be examined for both filtration and comfort performances. Nine were microporous fabrics (MP), 10 were multilayered nonwoven fibrous media (SMS) and one was a flash spun material (FS). To assess their filtration performances, fabrics were challenged in a benchtop wind tunnel with a 20–3,000 nm diameter sodium chloride aerosol at three low fabric face velocities (0.05, 0.15, 0.3 cm/sec). Airflow resistance and water vapor transmission rate were also measured to provide indications of comfort for the wearer. The penetration results led to the classification of the 20 fabrics into distinct groups of filtration efficiency. The data were analysed based on the porous media characteristics (thickness, fiber diameter, porosity, etc.). MPs were the most efficient fabrics, and SMSs showed a wide range of performances, mostly due to variations in the thickness of the filtering layer as well as to the fabric treatment. Measurements of airflow resistance and water vapor transmission rates revealed major differences between MPs and FSs and SMSs. This highlights the potential of some SMS fabrics to meet a compromise between protection and comfort.

### KEYWORDS

Aerosols; chemical protective clothing; filtration; non-woven

## Introduction

Workers are occupationally exposed to chemical and physical agents through inhalation and skin contact. Contrary to exposure via inhalation, no occupational exposure limits (OEL) are defined for dermal exposure.<sup>[1]</sup> At the moment, some chemicals are given “Skin Notations (SK)”<sup>[2]</sup> based on a hazard assessment, methods of which can vary from country to country.<sup>[3]</sup> The National Institute for Occupational Health and Safety (NIOSH) has recently reviewed its strategy to assign SKs to chemicals and better communicate the hazards of chemical exposure to the skin.<sup>[2]</sup>

With or without SKs, some chemicals present as aerosols in workplaces can be harmful, such as causing contact dermatitis.<sup>[4]</sup> This is the case for aerosols made of metals<sup>[5,6]</sup> (beryllium, nickel, silver, mercury,

gold) or glass fibers.<sup>[4,5]</sup> Beside the nature of the aerosols, their size can also be a major factor to consider when performing a risk assessment. Although scarce in number, existing studies warn about nanoparticle toxicity.<sup>[7–10]</sup> It has also been shown that nanoparticles could be absorbed by the skin.<sup>[7]</sup>

To prevent skin exposure to these particles, some chemical protective clothing might be recommended for workers. According to ISO 16602,<sup>[11]</sup> those chemical protective clothing designed to protect against solid aerosols are referred to as “Type-5” and must comply with the performance requirements described in the ISO standard 13982-1.<sup>[12]</sup> Chemical protection is evaluated by measuring the total particle inward leakage. This consists in measuring mass-based particle concentration inside and outside a protective

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clothing worn by a subject performing exercises in an environmental chamber.<sup>[13]</sup>

Although such an approach is relevant for standardization, it lacks the consideration of important factors that could inform on the particle penetration pathways (e.g., seams, zipper, material, skin/clothing interface). Also, as there are no classes of performance for this type of protective clothing, it is impossible to compare between different Type-5 protective clothing based on the chemical protection they provide to the wearer. Finally, these standards do not require any physiological measurement of the wearer, making it difficult to choose a specific Type-5 protective clothing based on both comfort and protection.

Few studies have been conducted to improve our understanding of the determinants of the protection levels provided by particle-proof protective clothing, Type-5 certified or not. These studies first investigated fabrics by performing filtration experiments, where aerosol particles were pulled through a clothing sample while monitoring the particle concentration upstream and downstream.<sup>[14,15]</sup> A limited number of non-woven and woven fabrics were tested (hairnets, cleaning cloths, lab coats, protective clothing).<sup>[16,17]</sup> The fabric face velocities in such experiments ranged from 0.25–0.6 cm/s.<sup>[14–16]</sup> It especially appeared that cotton woven fabrics are not suitable for dermal nanoparticle protection and that non-woven materials should be preferred. Some filtration experiments performed on seams and zippers<sup>[15]</sup> highlighted the importance of these points of entry for nanoparticles.

Assuming that the filtration approach was not simulating the field use of protective clothing, some authors<sup>[16,18]</sup> developed an experimental setup to study penetration of particles when no air was pulled through the fabric, called the “diffusion through” method. Although limited to three protective clothing fabrics (one from a Type-5 certified clothing), these studies highlighted a possible penetration of nanoparticles under pure diffusional conditions. Some other authors<sup>[17]</sup> developed a closed-loop wind tunnel to measure the penetration of submicron particles at different wind speeds. While this setup could mimic real workplace exposure (one wind speed in the tunnel associated with different natural infiltration flow rates depending on the type of fabric), the authors adjusted the wind speed to reach the same fabric face velocities for all fabric samples (0.009, 0.018, and 0.027 cm/sec). Thus, the implementation of this method equaled a classical filtration approach at low fabric face velocities.

This literature review highlights the fact that the ISO standardized test for Type-5 protective clothing does not provide enough knowledge that could allow workers finding the right balance between comfort and the protection they need. It also shows the paucity of data in the literature regarding the performance of Type-5 protective clothing fabrics. Finally, it is worth pointing out that all the previously cited studies dealt with particles smaller than 500 nm (nanoparticles and sub-micron particles), while the Type-5 certification assesses the clothing performances using an aerosol with a broad particle size distribution, from 20–2,000 nm. Therefore, this project aimed at studying and explaining the performances of a large panel (20) of protective fabrics against solid aerosols. To do so, the fabric protection performances were evaluated for a broader particle size range (20–3,000 nm). In addition, three very low superficial velocities were used to simulate as closely as possible real work conditions. Measurements of fabric thermal comfort-related properties (airflow resistance and water vapor transmission rate) were also performed to discuss the balance between comfort and protection. These performances were analyzed based on the fabric characterization and the filtration theory.<sup>[19]</sup>

## Materials and methods

### Fabrics

Twenty common fabrics used for the manufacturing of protective clothing against solid aerosols were chosen (Table 1). Ten of them were made of an assembly of at least one meltblown layer (M layer) between two spunbonded layers (S layers), usually

**Table 1.** Selected Protective Clothing.

Protective clothing	Type of fabric	Material <sup>A</sup>	Abbreviations
3M 4510	MP	PE/PP	3M 4510
3M 4520	SMS	PP	3M 4520
3M 4530	SMS	PP	3M 4530
3M 4540	MP	PE/PP	3M 4540
Kimberly-Clark A10	SMS	PP	KC A10
Kimberly-Clark A20	SMS	PP	KC A20
Kimberly-Clark A30	SMS	PP	KC A30
Dupont Tyvek Xpert	FS	HD-PE	Tyvek
Dupont Proshield NexGen	MP	PE/PP	DPN
Honeywell North Gen Pro	SMS	PP	NGP
Honeywell North Gen Air	MP	PE/PP	NGA
Käppler ProVent 10000	MP	PE/PP	KP 10000
Lakeland Safeguard	SMS	PP	LSG
Lakeland Micromax NS	MP	PE/PP	LMX
Portwest ST 30	SMS	PP	ST 30
Portwest ST 40	MP	PE/PP	ST 40
Alphatec Microchem 1500	SMS	PP	M 1500
Alphatec Microchem 1500FR	SMS	PP	M 1500FR
Alphatec Microchem 1800	MP	PE/PP	M 1800
Alphatec Microchem 2000	MP	PE/PP	M 2000

APE: Polyethylene / PP: Polypropylene / HD: High Density

referred to as SMS (Spunbond/Meltblown/Spunbond). Nine of them were an assembly of one or several spunbonded layers with one microporous film, usually referred to as microporous (MP). The remaining fabric was a single layer made of flash-spun fibers (FS).

### **Measurement of particle penetration through fabrics**

#### **Wind tunnel**

A 1.4 m long, open-jet wind tunnel with a 400 cm<sup>2</sup> cross-section (20 x 20 cm) was built. The wind speed in the tunnel ( $U_T$ ) generated by a fan (FX 5 XL, Fantech, Sarasota, FL, USA) was about 0.3 m/sec (720 L/min). A 17 cm diameter circular penetration cell, 15 cm long was placed in the wind tunnel, perpendicular to the airstream, to secure fabrics to be tested. The area of this 17 cm sample holder represents 56.7% of the tunnel cross-section. Details about this experimental setup are reported in online supplemental materials (Figure S1).

The sodium chloride (NaCl) test aerosol was generated by a six-jet Collison Nebulizer (BGI by Mesa Labs, Butler, NJ, USA) using a 2.7% NaCl solution at 2.07 bars (30 PSI). It was charge neutralized (Aerosol neutralizer 3012, TSI, Shoreview, MN, USA) and dried with silica gel before being injected into the tunnel 65 cm downstream of the fan, through two face-to-face holes, and perpendicularly to the wind direction. The investigated particle sizes ranged from 20–3,000 nm. The particle size distribution of the generated aerosol is presented online supplemental materials (Figure S2). It was measured with a Scanning Mobility Particle Sizer (SMPS) for particles smaller than 600 nm in diameter (SMPS 3936, TSI, Shoreview, MN, USA) and an Aerodynamic Particle Sizer (APS) for particles between 600 and 3,000 nm (UVAPS 3314, TSI, Shoreview, MN, USA). The cross-sectional uniformity of the air velocity and particle concentration was verified following the guidelines of ASHRAE standard 52.2-2012<sup>[20]</sup> (Tables S1 and S2 in online supplemental materials).

#### **Fabric face velocities for testing**

A modeling study of air velocities around a cylinder supposed to represent the human body<sup>[21]</sup> showed that fabric face velocities for highly permeable clothing materials do not exceed 0.8 cm/sec for wind speeds up to 1.4 m/sec. Another study<sup>[22]</sup> showed that 85% of air velocities in indoor workplaces (e.g., asbestos removal enclosure, bakery, laboratory, wood

cutting area) were below 0.3 m/sec. According to the results of Brassler,<sup>[20]</sup> such a wind speed would lead to a fabric face velocity of 0.17 cm/sec for highly permeable fabrics. Thus, fabric face velocities were set at 0.05, 0.15, and 0.30 cm/sec for testing the penetration of particles through the fabrics.

#### **Penetration measurements.**

During penetration tests, relative humidity and temperature were about 25% and 20 °C, respectively. The previously described SMPS/APS coupling was used to measure particle concentrations and distributions upstream and downstream of the tested fabrics. To compensate for low fabric face velocities, a flow of clean compressed air (Flowmeter Model 4043, TSI Inc., Shoreview, MN) was added to the sample flow to reach the set points of both SMPS and APS (0.3 and 5 L/min, respectively).

The upstream and downstream particle-size distributions were measured at the center of the tunnel cross-section, with a sampling probe approximately located 20 cm before the fabric set on the penetration cell and 7 cm after the fabric, respectively. The filtration performances are expressed in terms of collection efficiency. Since only protective clothing fabrics were tested in this study, the collection efficiency will be referred to as protection efficiency in this article. The protection efficiencies were calculated based on the upstream and downstream concentrations measured with the previously described SMPS/APS coupling for each size bin of these particle counters. The sequence of this upstream and downstream sampling was based on standard EN 779,<sup>[23]</sup> dedicated to establishing the performance of filters (Table S3 in online supplemental materials). For each fabric, three samples were tested at the three selected fabric face velocities.

#### **Measurement of comfort indicator**

In this study, two fabric parameters considered to be indicative of comfort for the wearer were chosen. The first one is the airflow resistance representing the air permeability of a fabric. Thus, the lower the airflow resistance, the greater the chances of comfort. The other fabric parameter taken into account for comfort evaluation is the water vapor transmission rate representing the moisture permeability and thus the ability of a fabric to evacuate the human-source moisture. The water vapor transmission rate must be maximized to improve the level of comfort.

**Air permeability: Airflow resistance**

The pressure drop generated by a porous media is described by Darcy's law as:

$$\Delta P = \frac{1}{K} \cdot \mu \cdot U_f \cdot Z, \quad (1)$$

where  $\Delta P$  is the pressure drop (Pa),  $K$  is the intrinsic permeability of the porous media material ( $\text{m}^2$ ),  $\mu$  is the dynamic viscosity of the carrier fluid (Pa·s),  $U_f$  is the fabric face velocity (m/s), and  $Z$  is the thickness of the porous media (m). Since pressure drop is a function of both intrinsic permeability and media thickness, the ratio of these two properties,  $Z/K$ , was used to compare different media types. This ratio will be referred to as the hydraulic resistivity. According to Equation (1), the hydraulic resistivity can be easily calculated after measuring the pressure drop generated by a known airflow rate through a fabric of known area. The pressure drop measurements were performed with a 0-250 Pa and a 0-1000 Pa sensor interfaced with a data logger (Almemo 2290, Ahlborn, Holzkirchen, Germany) for the SMS fabrics and the Tyvek. Due to their higher airflow resistance, a 0-5000 Pa inclined differential manometer (Type 4, Airflow developments, High Wycombe, UK) was used for the microporous fabrics. The airflow rate was measured with a 0-20 L/min mass flowmeter (4140, TSI Inc., Shoreview, MN).

**Moisture permeability: Water vapor transmission rate**

The water vapor transmission rate expressed in  $\text{g}/\text{m}^2/\text{day}$  was measured following the ASTM-like F2298 standard.<sup>[24]</sup> This method uses a dynamic moisture permeation cell (DMPC) exposing the two faces of a  $10 \text{ cm}^2$  sample to co-current airflows differing from each other by their relative humidity. The difference in relative humidity was 90% (95% – 5%). A pressure difference is also applied between the two faces of the garments. This pressure difference is increased gradually from -150 Pa to 150 Pa. Then, at the exit of the DMPC, the relative humidity of the two airflows is measured again, the changes in relative humidity in these flows enabling the calculation and the plotting of a water vapor flux as a function of the pressure difference. The y-axis intercept of the obtained curve is considered to be the water vapor transmission rate. This data is therefore representative of the diffusional water vapor flux.

**Fabric characterization**

Except for the Tyvek, all the fabrics are composed of several layers, only one of which acts as an efficient particle filter: the upper microporous film for MP garments and the middle meltblown layer for the SMS fabrics. Thus, the characterization of the different materials can be considered at two levels: the whole fabric and the filtering layer.

**Fabric thickness**

The total thickness of the protective clothing materials was measured following standard CAN/CGSB-4.2 No. 37-2002.<sup>[25]</sup> This standard, developed for compressible textile fabrics, consists in applying an arbitrary pressure (1,000 Pa) on the tested sample between plane surfaces.

**Meltblown layer thickness**

It was not possible to use the same standard for measuring the thicknesses of meltblown layers because layers of the SMS assemblies cannot be separated without being damaged or modified. The meltblown layer thicknesses were then measured on cross-sectional images of SMS samples. These photos were taken with a stereomicroscope (SMZ-18, Nikon Instruments Inc., Tokyo, Japan) providing a large enough observation distance and magnification, i.e., 135x. For these observations, the samples were inserted between microscope and cover slides to hold them without significant compression. After acquisition, the images were automatically analyzed with a MATLAB (Mathworks, Natick, MA) code detecting and measuring the M layer thickness.

**Fiber diameter**

Fiber diameters were measured for the SMS fabrics and spunbonded layer of the microporous materials. The measurements were performed using photographs taken by optical microscopy (Nikon Eclipse E400, Nikon Instruments Inc., Tokyo, Japan) set at 400x magnification. Some 100 measurements per fabric were performed with the ImageJ software (National Institutes of Health, Bethesda, MD). In the case of the SMS materials, measurements were performed on the two spunbonded layers (outer and inner layers) and on the M layer.

**Fabric porosity**

Once the fabric thickness is known, the fabric porosity can be calculated by measuring the surface density and the density of the fabrics using standards CAN/CGSB-4.2 No./N° 5.1-M90<sup>[26]</sup> and ASTM D792-

08,<sup>[27]</sup> respectively. The fabric porosity is given by Equation (2):

$$\epsilon_T = 1 - \frac{W}{(\rho_f \cdot Z_T)}, \quad (2)$$

where  $W$  is the surface density ( $\text{kg/m}^2$ ),  $Z_T$  is the thickness of the fabric (m), and  $\rho_f$  is the fabric material ( $\text{kg/m}^3$ ).

### Meltblown layer porosity

The calculation of the meltblown layer porosity were based on the use of the Davies pressure drop equation<sup>[28]</sup> for fibrous media (Equation (3)):

$$\begin{aligned} \Delta P_M &= \frac{1}{K_M} \cdot \mu \cdot U_f \cdot Z_M \\ &= \frac{64 \cdot (1 - \epsilon_M)^{\frac{3}{2}} \cdot (1 + 56 \cdot (1 - \epsilon_M)^3)}{d_{f,M}^2} \cdot \mu \cdot U_f \cdot Z_M, \end{aligned} \quad (3)$$

where  $\Delta P_M$  is the M layer pressure drop (Pa),  $K_M$  the M layer intrinsic permeability ( $\text{m}^2$ ),  $\epsilon_M$  the M layer porosity,  $d_{f,M}$  the M fiber diameter (m),  $\mu$  the dynamic viscosity (Pa.s),  $U_f$  the fabric face velocity (m/s), and  $Z_M$  the M layer thickness (m).

Since  $d_{f,M}$ ,  $U_f$ ,  $Z_M$ , and  $\mu$  are known, the M layer porosity  $\epsilon_M$  could be calculated as long as the M layer pressure drop  $\Delta P_M$  could be measured. Since the meltblown layers could not be separated from the S layers,  $\Delta P_M$  could not be measured directly. It was hypothesized that, since the particle collection is supposed to be predominantly due to the M layer, the pressure drop of the fabric was also being predominantly due to the M layer ( $\Delta P_M = \Delta P_{SMS}$ ).

This hypothesis could be verified using Davies' model (Equation (3)) to express the measured fabric pressure drop as the sum of the pressure drops in the S and M layers (Equation (4)):

$$\begin{aligned} \Delta P_{SMS} &= \frac{64 \cdot (1 - \epsilon_M)^{\frac{3}{2}} \cdot (1 + 56 \cdot (1 - \epsilon_M)^3)}{d_{f,M}^2} \cdot \mu \cdot U_f \cdot Z_M \\ &+ \frac{Z_S}{K_S} \cdot \mu \cdot U_f, \end{aligned} \quad (4)$$

where  $\Delta P_{SMS}$  is the whole material measured pressure drop (Pa),  $K_S$  the intrinsic permeability ( $\text{m}^2$ ) of the two S layers, and  $Z_S$  their thickness (m). With the terms  $d_{f,M}$ ,  $U_f$ ,  $Z_M$ , and  $\mu$  being known,  $Z_S$  being calculated from the difference between the whole material, and the M layer thicknesses; only  $K_S$  has to be determined to evaluate  $\epsilon_M$ , the M layer's porosity. The  $K_S$  was measured following the method described earlier for the airflow resistance evaluation, using five separated S layers from microporous films (M 1800, M 2000, ST 40, NGA, and LMX). Thus, this approach

assumed that the S layers from all the fabrics, SMS and MP, were similar. This assumption was supported by our measurements, showing that 15 out of the 18 garments have S fiber diameters ranging from 17–20  $\mu\text{m}$ .

A good agreement between  $\epsilon_M$  values obtained from Equations (3) and (4) would tend to confirm the assumption of a negligible contribution from the S layer to the SMS fabrics pressure drop.

### Pore size distribution

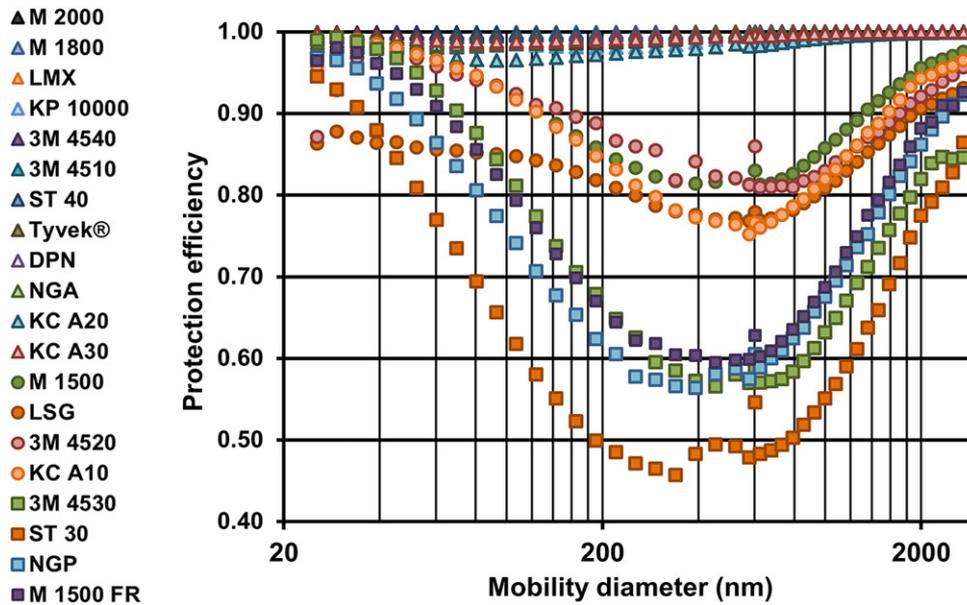
The pore size distribution of the whole material was measured according to standard ASTM D6767-16,<sup>[29]</sup> relative to pore size characterization of geotextiles by capillary flow test. It indicates the pore size below which there is a defined pore fraction (98%, 95%, 90%, 85%, 60%, 50%, 30%, 15%, 10%, and 5%). The smallest pore diameter measurable by this method is 1  $\mu\text{m}$ .

## Results and discussion

### Protection efficiency

When measured at three different fabric face velocities, the results of the measured protection efficiencies highlighted the separation of the 20 protective fabrics into three distinct groups: low (Group A – square markers in Figure 1 – minimum protection efficiency around 0.50), medium efficiency (Group B – circular markers in Figure 1 – minimum protection efficiency around 0.75), and very high efficiency (Group C – triangular markers in Fig. 1 – minimum protection efficiency around 0.95). Figure 1 illustrates these groupings at a fabric face velocity of 0.3 cm/sec.

According to Figure 1, Groups A and B are composed of four SMS fabrics (3M 4530, M 1500FR, ST 30, NGP and 3M 4520, M 1500, KC A10, LSG) and Group C is a combination of two SMS, nine microporous and one flash spun fabric (KC A20, KC A30, ST 40, M 1800, M 2000, KP 10000, LMX, DPN, NGA, 3M 4510, 3M 4540, Tyvek). Two other facts were also noticed on Figure 1: (1) the very flat efficiency curve of the LSG in the diffusional regime and (2) the significantly lower efficiency of the ST 30 fabric compared to the other Group A materials. This was observed for the three fabric face velocities. The composition of the three groups of protection efficiency remaining unchanged for all the tested fabric face velocities, a more convenient way of displaying and comparing the results was to represent the average protection efficiency of each group with the standard deviation as error bars (Figure 2). For Groups A and



**Figure 1.** Protection efficiency of the 20 protective clothing (Fabric face velocity 0.3 cm/sec – Square markers: Gr. A / Circular markers: Gr. B / Triangular markers: Gr. C).

B, the typical particle filtration medium behavior was observed, i.e., an increase in collection efficiency as the fabric face velocity decreases, especially for the smallest particles due to the enhancement of the collection by Brownian diffusion, as well as an increase of the most penetrating particle size (MPPS) still between 300 nm and 700 nm.

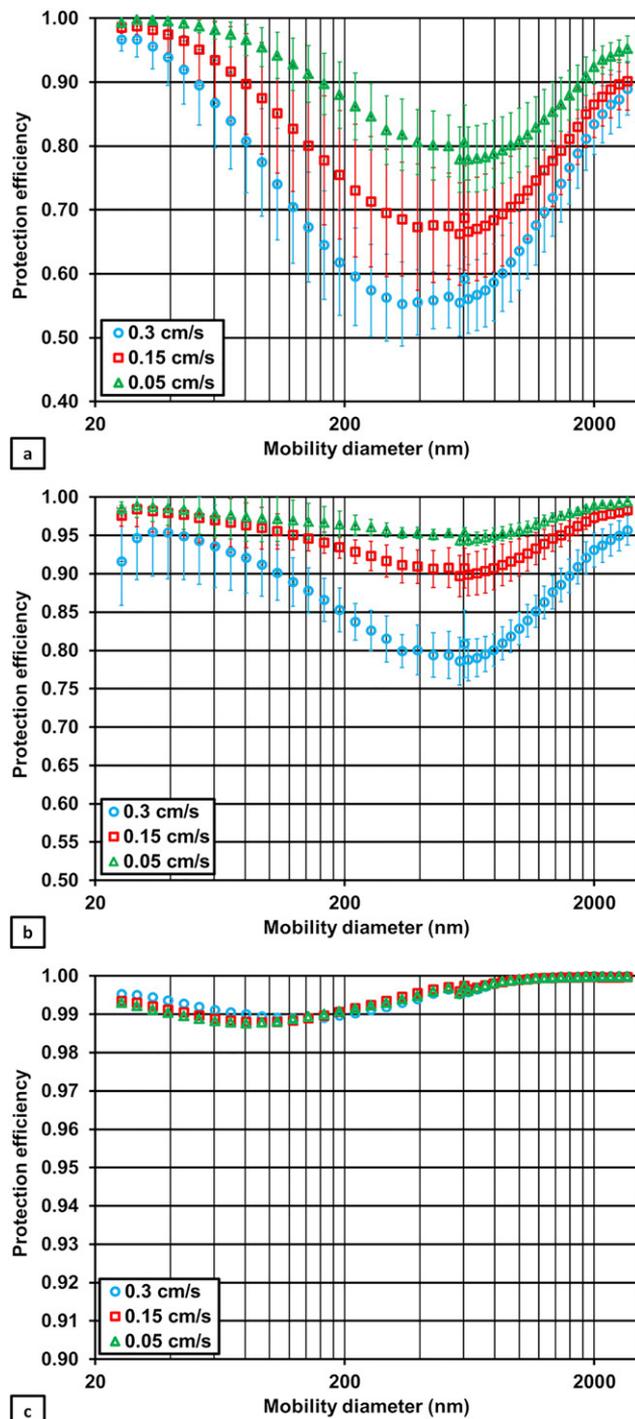
This is more visible on [Figures 3a and 3b](#), showing the minimum protection efficiency and the MPPS of all A and B cluster materials. However, [Figure 3b](#) reveals an exception, the LSG MPPS appeared to strongly decrease at low fabric face velocity. Nevertheless, this last point must be tempered by the fact that these are mathematical MPPS obtained by derivative function inversions introducing uncertainties for this kind of flat efficiency profile.

Group C being composed of various kinds of fabrics, its behaviour, except concerning its close to 1 protection efficiency, cannot be precisely described by this clustered display. As shown in [Figure 4a](#), six of the nine MP materials (3M 4510, DPN, LMX, M 1800, M 2000, ST 40) showed a slight drop in the minimum protection efficiency instead of an increase, two remained constant (3M 4540, NGA) and only one (KP 10000) behaved as expected with an increase of its minimum collection efficiency as the fabric face velocity decreased.

If the minimum protection efficiency of microporous fabrics often did not follow the expected trend, their MPPS increased as the fabric face velocity decreases as predicted by the filtration theory. However, MPPS values were significantly smaller than

those obtained for classical fibrous media such as the SMS fabrics of the A and B Groups. In this article, the term “classical fibrous media” is used to describe fibrous media that do not provide enhanced collection efficiency by electrostatic effects such as electret filters. Indeed, with the exception of one microporous fabric (KP 10000), all the MPPS were below 250 nm. For the other types of materials belonging to Group C [one flash spun (Tyvek) and two SMS fabrics (KC A20 and KC A30)], [Figures 4a and 4b](#) highlight an expected qualitative behaviour, i.e., a decrease in protection efficiency and MPPS values as the fabric face velocity increases. Quantitatively, MPPS values were again smaller than those of classical fibrous media (below 200 nm).

Because of the lack of identification of tested fabrics in the literature, an accurate comparison of their performances with the results of this study appears to be difficult. Indeed, previous studies dealt with a narrower particle size range,<sup>[16–18]</sup> larger fabric face velocities, or expressed the protection efficiency as global and not size-dependent.<sup>[15]</sup> Nevertheless, the results of two studies could partially be compared to those obtained in this work. Among the 10 samples tested by Gao et al.,<sup>[17]</sup> one could be identified as a fabric (SMS) from a coverall protective clothing. In addition, some of their fabric face velocities are very close to those used in this work: 0.25 cm/sec and 0.37 cm/sec. For these velocities and for particles ranging from 30–500 nm in diameter, the results of Gao et al. appeared to compare satisfactorily with the protection efficiency of the Group A measured at 0.3 cm/sec.



**Figure 2.** Protection efficiency of the three groups of Type-5 protective clothing at three different fabric face velocities (a: Gr. A, b: Gr. B, c: Gr. C).

Despite a larger fabric face velocity, these article results are also consistent with those of Salah et al.<sup>[14]</sup> (particle size range from 15–400 nm and fabric face velocity of 0.435 cm/sec). Thus, Salah et al. highlighted the very high efficiency of microporous and flashspun fabrics. Their data for two SMS fabrics are also in agreement with this article, showing possibly a Group

B SMS having a lower efficiency because of a larger fabric face velocity and a Group C SMS with a very high level of protection and a MPPS around 100 nm.

### Comfort indicators

#### Airflow resistance

As stated in the materials and methods sections, hydraulic resistivity was chosen as an indicator of the fabric air permeability. Thus, the lower the airflow resistance, the greater the chances of comfort. Similar to the protection efficiency, three groups of airflow resistance were revealed (Table 2). These groups are somewhat different and correspond to the three types of protective clothing materials: Flash Spun (FS), Microporous (MP) and Spunbond/Meltblown/Spunbond (SMS). As intuitively thought, microporous fabrics having the highest protection efficiencies appear to also have, by far, the highest hydraulic resistivity, i.e., about 10,000 and 100 times greater than the SMS and flash spun materials, respectively.

#### Water vapor transmission rate

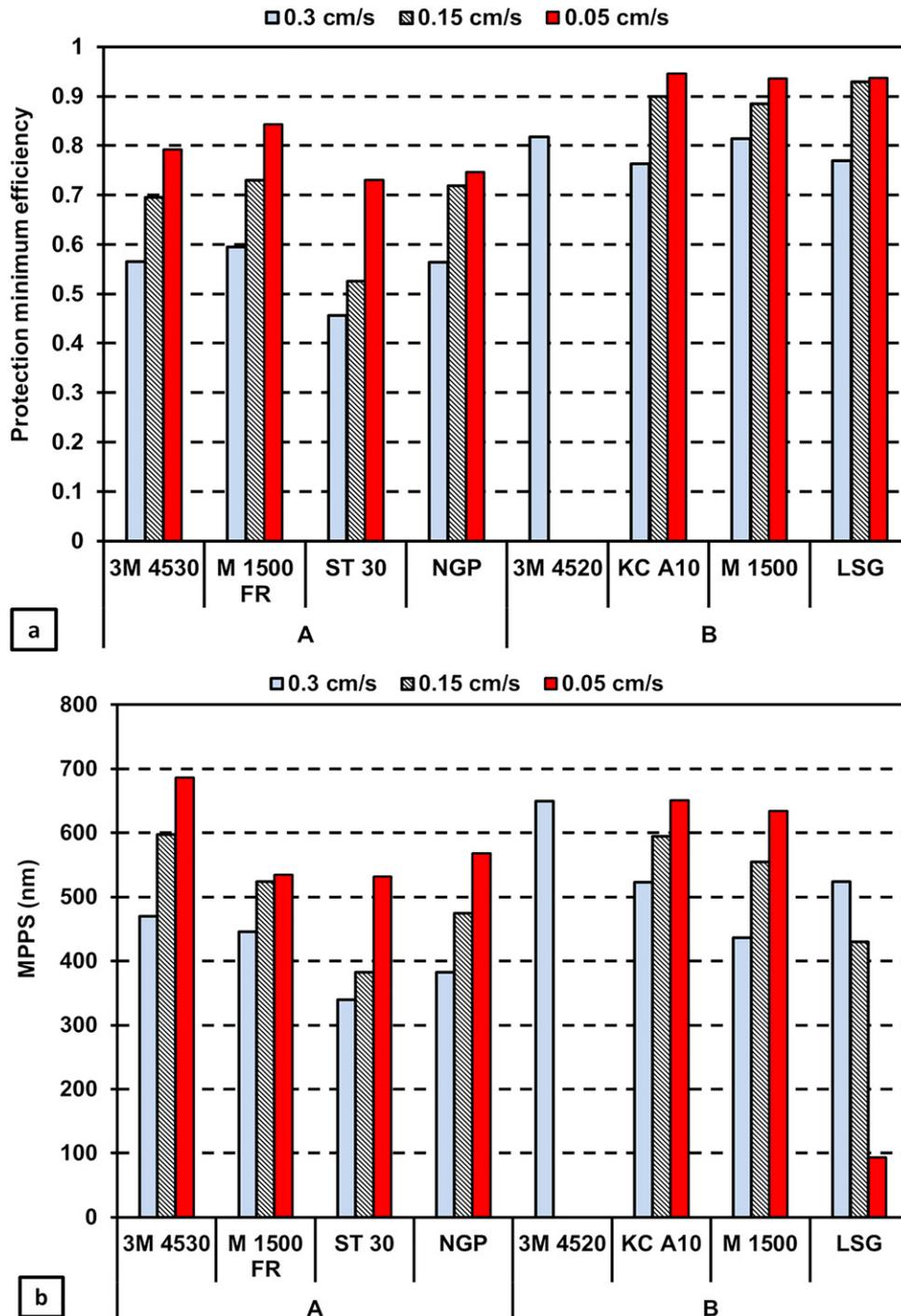
By analogy with the airflow resistance, water vapor transmission rate was chosen as an indicator of the human-source moisture control. According to this definition, this parameter must be maximized to improve the level of comfort. The moisture control parameter appeared almost to correlate with air permeability evaluation (Table 2). Indeed, SMS fabrics generating the smallest airflow resistance have a greater water vapor transmission rate and MP materials appear again by far to be the least permeable to water vapor. It must also be noticed that, as opposed to airflow resistance, the water vapor transmission rate of the FS material is of the same order of magnitude as the MP garments.

Only few studies provide information about comfort indicators. Nevertheless, once converted to hydraulic resistivity, the value of air permeability given by Gao et al.<sup>[17]</sup> for their SMS fabric correlates well with the results presented in Table 2 for the same kind of materials.

### Differences in protection efficiency

#### Groups A (except ST 30) and B (except LSG)

Groups A and B show low and medium protection efficiency, respectively, and are only composed of SMS fabrics. From the characterization of the filtration layer (M layer) of these fabrics, no clear trend emerged concerning the factors governing the



**Figure 3.** (a) MPPS Protection efficiency of A and B cluster garments; (b) MPPS for A and B cluster garments. (For the 3M 4520 fabric, only data at 0.3 cm/s are available because of an experimental issue.)

protection efficiency. Thus, for these two groups, the M fiber diameter ranges from 2–2.5  $\mu\text{m}$  (Figure 5a) without exhibiting a decreasing pattern from Group A to B, which would increase the collection efficiency. The same absence of correlation was obtained regarding the estimated M layer porosity varying between 0.7 and 0.85 (Table 2) without systematically being lower for Group B. As for the M layer’s porosity, the

data in Table 2 show that the two methods used for its calculation give similar results, indicating, as mentioned previously, the negligible effect of the S layers on the SMS fabrics’ airflow resistance. The only parameter varying clearly in a similar way and which could explain the efficiency gap between Groups A and B appears to be the M layer thickness: close to 11  $\mu\text{m}$  and 16  $\mu\text{m}$  for Groups A and B, respectively

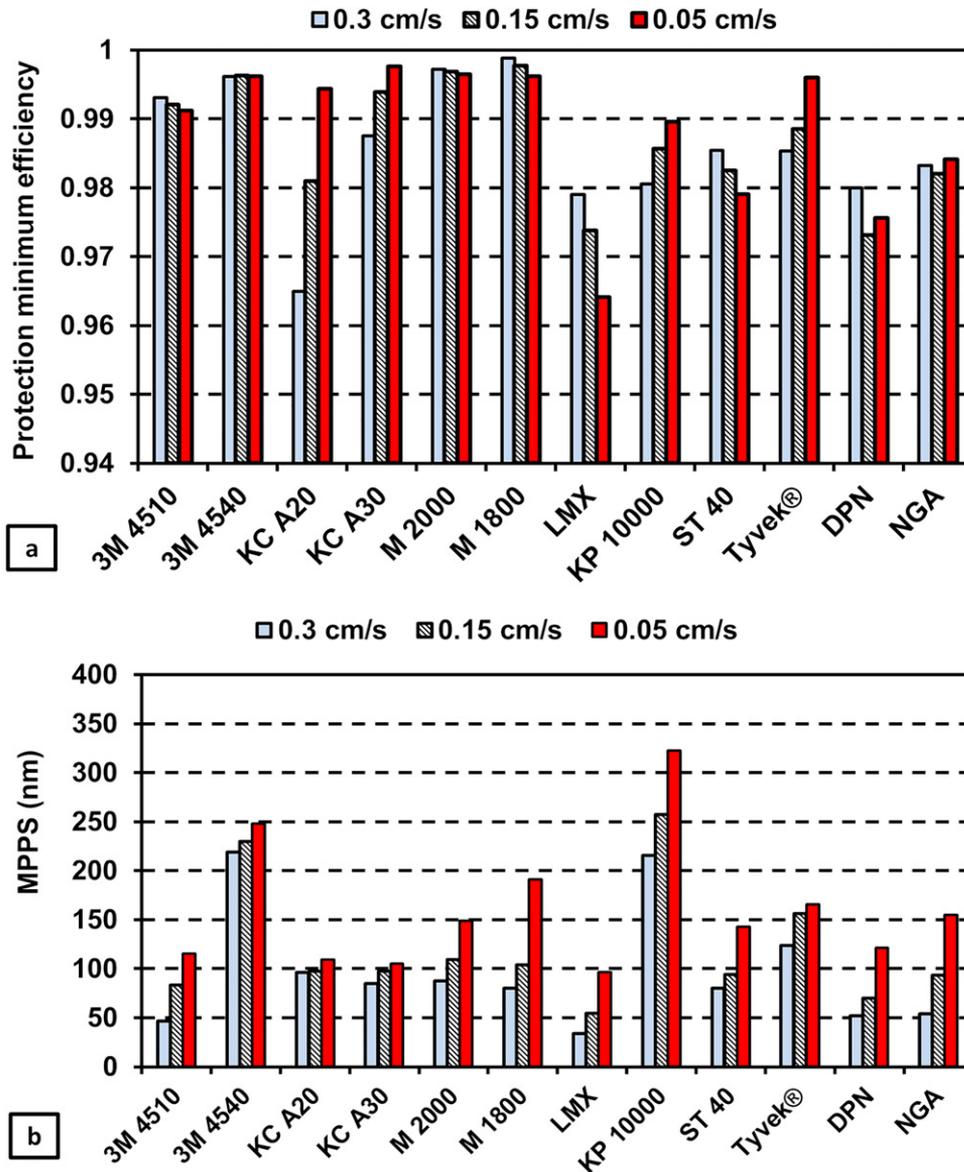


Figure 4. (a) MPPS Protection efficiency of C cluster garments; and (b) MPPS for C cluster garments.

(Figure 5b). On average, the M layer thickness differs by a factor of 1.5 from one group to another.

To verify whether this increase in M layer thickness could effectively cause the change in efficiency from Group A to Group B, the collection efficiency of a virtual protective fabric was calculated on the basis of the Group A mean efficiency, considering that no other parameters changed except for the M layer thickness. The equation used for this calculation is the global efficiency law of fibrous filters.<sup>[19]</sup> For Group A SMS, the protection efficiency  $E_A$  is given by:

$$E_A = 1 - \exp\left(-4 \cdot e_f \cdot \frac{1-\epsilon}{\epsilon} \cdot \frac{Z_{M,A}}{\pi \cdot d_f}\right), \quad (5)$$

where  $e_f$  is the single fiber collection efficiency,  $\epsilon$  the porosity of the fibrous media,  $d_f$  the fiber diameter

(m), and  $Z_{M,A}$  the M layer thickness (m). The same equation can be used to compute the virtual SMS efficiency,  $E_Y$ :

$$E_Y = 1 - \exp\left(-4 \cdot e_f \cdot \frac{1-\epsilon}{\epsilon} \cdot \frac{Y \cdot Z_{M,A}}{\pi \cdot d_f}\right). \quad (6)$$

All parameters remained unchanged between Equations (5) and (6) except for the introduction of the M layer thickness factor,  $Y$ , equal to 1.5 (ratio of the mean  $Z_{M,B}$  and  $Z_{M,A}$  values). By combining Equations (5) and (6),  $E_Y$  can be expressed as:

$$E_Y = 1 - (1-E_A)^Y. \quad (7)$$

If the difference in M layer thickness is indeed the main cause of the efficiency gap between Groups A and B, then  $E_Y$  should be close to Group B's mean

**Table 2.** Measurement results of hydraulic resistivity, water vapor transmission rate, M layer porosity and total fabric porosity of the 20 selected protective clothing.

VPC	Type, group	Hydraulic resistivity (/m)	Water vapor transmission rate (g/m <sup>2</sup> /day)	M layer porosity ( $\Delta PM = \Delta PSMS$ )	M layer porosity ( $\Delta PM = \Delta PS + \Delta PM$ )	Total fabric porosity
Tyvek®	FS, C	2.63E+09	5983	–	–	0.764
M 2000	MP, C	1.90E+11	6814	–	–	0.787
M 1800	MP, C	3.10E+11	3367	–	–	0.797
LMX	MP, C	6.52E+11	3721	–	–	0.777
KP 10000	MP, C	7.02E+10	6179	–	–	0.799
3M 4540	MP, C	1.28E+11	5831	–	–	0.772
3M 4510	MP, C	1.96E+11	5189	–	–	0.807
ST 40	MP, C	1.91E+11	4480	–	–	0.795
DPN	MP, C	2.70E+11	4895	–	–	0.810
NGA	MP, C	4.96E+11	2672	–	–	0.773
M 1500 FR	SMS, A	3.03E+07	13424	0.730	0.741	0.828
3M 4530	SMS, A	2.22E+07	14557	0.805	0.819	0.810
ST 30	SMS, A	2.66E+07	13052	0.703	0.715	0.834
NGP	SMS, A	2.37E+07	15311	0.773	0.786	0.847
LSG	SMS, B	7.41E+06	15081	0.848	0.889	0.849
3M 4520	SMS, B	2.59E+07	12948	0.812	0.822	0.851
M 1500	SMS, B	3.49E+07	12979	0.796	0.804	0.831
KC A10	SMS, B	2.01E+07	12508	0.826	0.839	0.851
KC A20	SMS, C	2.96E+07	14196	0.777	0.786	0.849
KC A30	SMS, C	4.96E+07	14339	0.731	0.738	0.839

collection efficiency. This can be observed in Figure 6 for a fabric face velocity of 0.3 cm/sec where mean relative errors do not exceed 10%. On this figure, the dashed purple curves correspond to the virtual material efficiencies considering the mean geometric standard deviation of the M layer thickness measurements leading to 1.44 and 1.59 as Y values. For fabric face velocities of 0.15 cm/sec and 0.05 cm/sec, this relative error is below 7% and 5%, respectively (see Figure S3 in supplemental information).

### LSG and ST 30 fabrics

Two SMS fabrics stood out of the general protection efficiency behavior observed for Group A and B: the LSG (Group B) and the ST 30 (Group A). LSG exhibits a flat protection efficiency profile in the diffusional regime and the submicron particle range. If no definitive explanation could be found yet, the fabric characteristics highlighted the unique structure of the LSG. The difference with the other SMS materials is especially noticeable in terms of S and M fiber diameters (Figure 5a). Indeed, LSG S fibers are between 25% and 50% larger compared to other fabrics and M fibers are about 50% larger than those of almost all SMS (except ST 30). These larger fiber diameters might be one of the reasons for the greater pore size of the LSG (two times larger than other SMS materials) showed in Figure 7.

These larger pores could partially explain the lower collection efficiency of the Brownian particles compared to other SMS of Group B, but also the lowest airflow resistance among all the tested clothing (Table 2). However, this larger pore size still does not explain

why only the Brownian particles collection efficiency seems to be altered and why the performances of the LSG belongs to Group B with medium efficiency. Indeed, all relevant parameters should imply equal (M layer thickness) or lower protection performances than the other Group B SMS (larger M layer porosity and M fiber diameter). A hypothesis to explain that behavior might be the presence of an unknown treatment of the fiber.

Although assimilated to Group A SMS, ST 30 exhibits protection performances significantly lower than the other three (M 1500FR, 3M 4530 and NGP), i.e., efficiencies lower by between 10 and 20%. This might be explained by the characterisation data. Indeed, for a same M layer thickness, ST 30 is made of the largest M fibers of the 20 tested fabrics, a larger fiber diameter not compensated for by a lower M layer porosity.

### Group C

**Microporous protective clothing.** As previously mentioned, Group C includes the three fabric types and exhibits very high protection efficiencies. It includes all the microporous fabrics, whose filtration layer is not made of fibers, but rather consists in a membrane with very fine pores. According to Figure 7, these pores are about 1 or 2  $\mu\text{m}$  in diameter, but they are certainly smaller given these values correspond to the measurement limit of the standard method used in this study. Indeed, slit shape pore dimensions as small as 20–40 nm wide by 200–400 nm long for this kind of microporous films were identified in the literature.<sup>[30,31]</sup> Added to these low pore sizes, the general

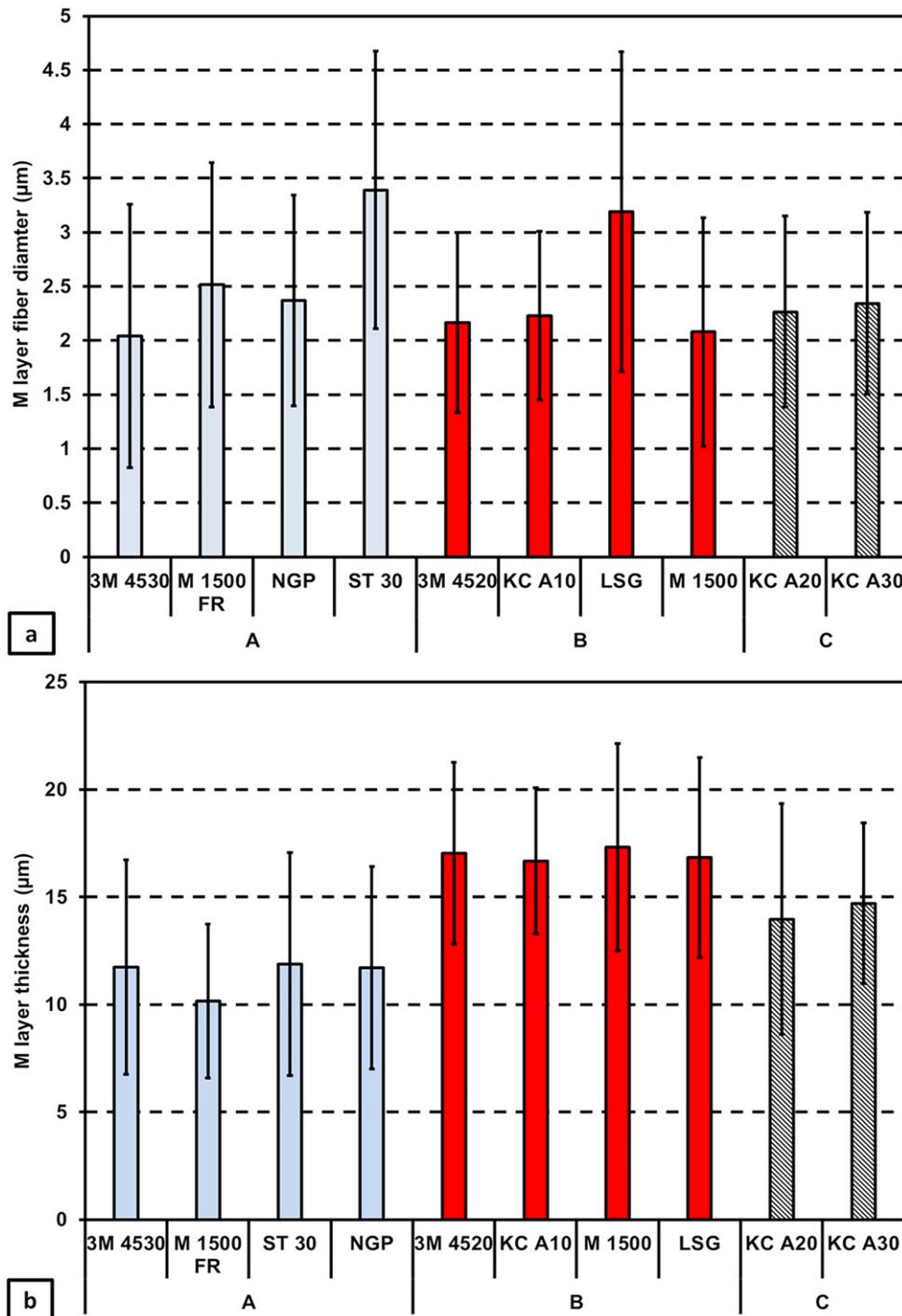


Figure 5. (a) M layer fiber diameter of SMS fabrics; and (b) M layer thickness of SMS fabrics.

lower fabric total porosity compared to the SMS materials (Table 2) also explains the high protection level of MP fabrics.

The pore size could also provide an explanation regarding the very small decrease or stability of the protection efficiencies with the decrease in fabric face velocity, observed for eight of the nine microporous garments and represented by the MPPS protection efficiencies shown on Figure 4a. The very small sized

pores, by generating very large pressure drops, could create a low-pressure atmosphere in the MP films. Indeed, using Darcy's law (Equation (2)) and the previously calculated MP fabrics' hydraulic resistivity, these pressure drops were found to be up to 17% of a normal atmospheric pressure for a fabric face velocity of 0.3 cm/sec. This could transform their internal solid fractions into low-pressure impactors due to a larger particle mean free path in air, increasing therefore by

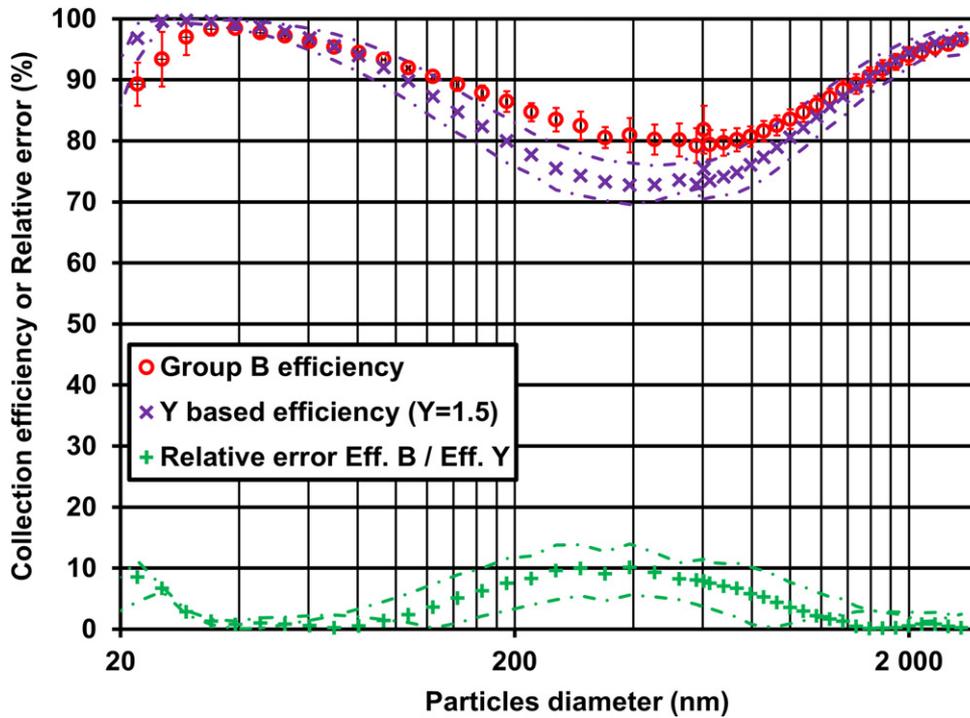


Figure 6. Comparison of the virtual protective clothing with the Group B fabrics assuming a M layer thickness of  $Y \times Z_{M,A}$  ( $Y = 1.5$ ) for a fabric face velocity of 0.3 cm/sec.

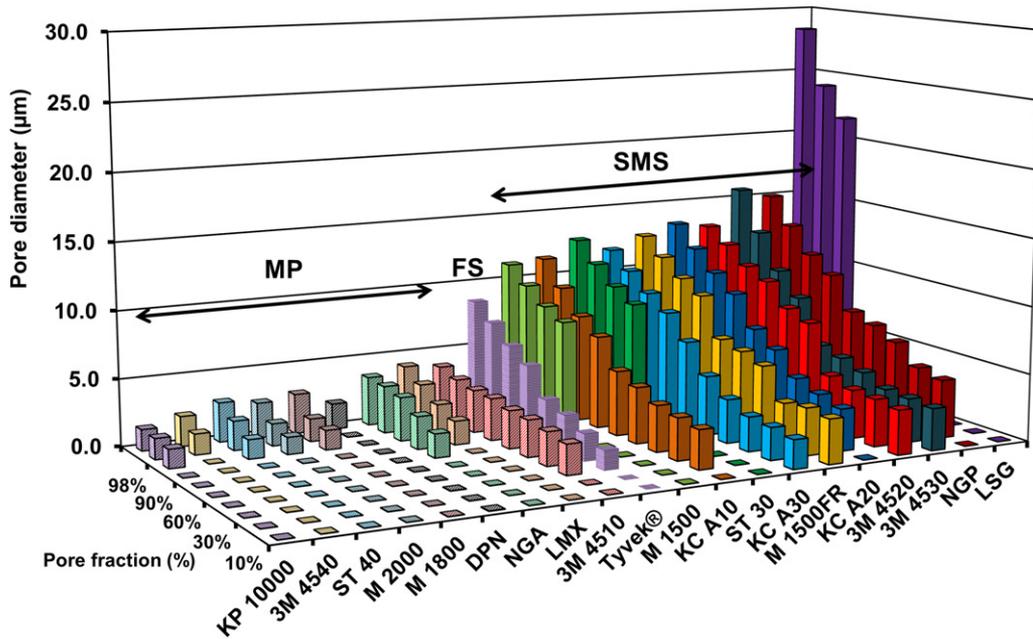


Figure 7. Pore diameter distribution of the 20 protective fabrics.

impaction the collection efficiency even of low inertia particles and thus compensating for the decrease in Brownian diffusion. According to the MP film pore size, impaction is also assisted by the high air velocity inside the pores and the very short impaction distances inside the MP films (between a few dozen and hundreds of nm). Consistent with this assumption,

and interestingly, the MP fabrics exhibiting this unexpected behaviour generate the larger pressure drops (mostly between 10 and 20% of a normal atmospheric pressure) while the KP 10000, showing an increase in collection efficiency as the fabric face velocity decreases, is the most air permeable MP material (pressure drop of about 4% of the normal atmospheric

pressure). The MP fabrics showing approximately constant collection efficiencies for the three selected fabric face velocities are intermediates in terms of pressure drop (between 10 and 5% of the normal atmospheric pressure). The assumption made previously could also be consistent with the observed low (mostly below 150 nm) and increasing MPPS as the fabric face velocity decreases. Indeed, the low-pressure impaction could preferentially enhance the collection of 200–600 nm diameter particles compared to the ultrafine particles (below 100 nm). Another contribution to this low MPPS could also be the sieving effect created by the very small pores.

Compared to SMS fabrics, the MP structural properties are also consistent with the results of the comfort-assessment measurements, namely, four orders of magnitude larger for airflow resistance and the water vapor transmission rate lower by almost half.

**Flash spun protective clothing (Tyvek).** FS material (Dupont Tyvek) is also included in Group C; it is also the only monolayer fabric, meaning its entire thickness, about 226  $\mu\text{m}$ , performs aerosol filtration. Since this material is not made of clearly definable fibers, only a larger useful filtration thickness, an intermediate pore size compared to MP and SMS fabrics and one of the lowest filtration layer porosities (about 76%) could explain its high level of protection efficiency (above 98.5%), but also its intermediate performance in terms of airflow resistance (about  $10^9 \text{ m}^{-1}$ ). Although this is also consistent with Tyvek having a lower water vapor transmission rate compared to SMS materials, these properties do not explain why almost no difference was observed with that of MP fabrics.

**Spunbond/meltblown/spunbond protective clothing.** The last two protective fabrics included in Group C are the SMS KC A20 and KC A30. From a characterization standpoint, these are not very different from the other SMS. Indeed, compared to SMS fabrics of Group B (except LSG), they show similar fiber and pore diameters, and M layer porosity and thickness leading to similar hydraulic resistivity, water vapor transmission rate and surprisingly, to very high protection efficiencies for Group C SMS (above 96%). The MPPS of the KC A20 and KC A30 fabrics, around 100 nm, tend to prove that these differences in protection efficiency are due to a particle collection enhancement by electrostatic effects.<sup>[32]</sup> This assumption is further reinforced by the manufacturer's technical specifications indicating a fiber treatment called "MICROFORCE."

### **Balance between protection and comfort**

Thanks to the comfort-assessment measurements, it was possible to discuss the balance between protection and comfort. Indeed, this study showed that two SMS fabrics, namely KC A20 and KC A30, offered all the comfort advantages of SMS materials, i.e., low airflow resistance and high water vapor transmission rate, while achieving the same satisfactory level of protection efficiencies as the MP or FS fabrics. Nevertheless, it is crucial to note this supposed compromise only holds for protection against solid aerosols and may not remain valid for any other kind of chemicals (for instance, liquid aerosols and vapours). Moreover, even if very low fabric face velocities were used in this study, it is likely that the air velocities in actual work settings could sometimes be even lower. Thus, in some cases, it is possible, for example, that garments of Group B may reach higher efficiencies while still providing a good level of comfort. It is also worth pointing out that the fabric protection efficiency is only a part of that of the entire clothing. Indeed, other characteristics could have a major effect on protection efficiency, such as seams, skin/clothing interfaces, and wear by abrasion or flexion. These aspects were part of the study and will be reported in a later article. Furthermore, movements of workers can be responsible for the so-called bellows effect which might create air convection, inward and outward of the protective clothing, altering both its protection and comfort. Thus, this quick assessment of compromise is essential, but it falls short of the multidimensional aspects of comfort. Further experimentations should be performed with human subjects at work wearing protective clothing made of different fabrics, to measure physiological strain, total inward leakage, and a subjective assessment of comfort.

### **Conclusions**

In general, for the three tested velocities, the results of the protection efficiency measurements highlighted the separation of the fabrics into three distinct groups (low, medium, and very high protection efficiency). The low and medium efficiency groups are only composed of SMS (Spunbond/Meltblown/Spunbond). The very high efficiency group gathers all the microporous fabrics, the Tyvek (flashspun fabric) and two SMS. Most results could be explained by the characterization of the fabrics. Indeed, the low and medium efficiency SMS and Tyvek performances were found to be mostly due to the filtration layer thickness, i.e., the meltblown one and the whole fabric, respectively. As

for microporous fabrics, submicronic pores provide efficiencies larger than 97%. Finally, the approximately 100 nm MPPS and the manufacturer's datasheets of the two most protective SMS, highlighted a probable fiber electrostatic treatment explaining their performances. Combined with the comfort-assessment measurements, a compromise could be proposed that takes into consideration both comfort and protection. Indeed, these two very efficient SMS fabrics exhibit also a low level of airflow resistance and a high level of water vapor transmission rate. However, this compromise has certain caveats. It only holds for protection against solid aerosols and not against other kinds of chemicals (namely, liquid aerosols and vapour).

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